

ILLUMINATION DESIGN OF ULU MOSQUE

OSMAN GUVEN ACAR 88002 DEPARTMENT OF ELECTRICAL AND ELECTRONIC ENGINEERING

GRADUATION PROJECT SUPERVISED BY : PROF. HALDUN GURMEN

EASTERN MEDITERRANEAN UNIVERSITY

FAMAGUSTA

T.R.N.C





- 1001 0001
- INTRODUCTION

CHAPTER ONE

- OUTDOOR ILLUMINATION
 - I) PLANNING
 - II) CARRIYING OUT A FLOODLIGHTING PROJECT

i- Direction of view

- ii- Distance
- iii- Surroundings and background
 - iv- Obstacles
 - v- Setting up the light sources
 - vi- Form of the building

III) ARCHITECTURE OF THE FACADE

- i- Flat facades
- ii- Facade with vertical lines
- iii- Facade with horizontal lines
 - iv- Facades with projections
 - v- Facades with recessed parts

vi- Mirror effects

- IV) SURFACE MATERIAL OF THE FACADE
 - V) SHAPE OF ROOFS
- VI) SELECTION OF THE LEVEL OF ILLUMINATION

CHAPTER TWO

- I) EQUIPMENTS USED IN FLOODLIGHTING
- i- Projector
- ii- Armature
 - II) UNITS AND DEFINITIONS
- III) METHODS OF CALCULATION
 - i- Lumen Method
 - ii- Direct Method
 - IV) CALCULATION OF THE PROJECT
 - VI) RESULTS OF CALCULATIONS
 - VI) COMPUTER PROGRAM

CHAPTER THREE

- I) VIEWS OF THE BUILDING
- II) INSTALLATION PLAN
- III) COST OF THE PROJECT
- DISCUSSION AND CONCLUSION
- APPENDIX

A C K N O W L E D G E M E N T S

I would like to have a special thanks to my supervisor Prof.Haldun GURMEN for providing me all the required documents and directing me through my project.

Also I would like to thank to my friend Mr. Zafer YUKSEL for his helps to prepare this project. There is no broken that freeding being a spectrum of the sector of the s

Lorenze Unit when floosile Phoneirgelon of some of belonding and other loss of the second some the belonding and the second second second be and condition and the floosile of second second be and some shift were less for or sectores there share adound particle prove contract in this way sign and the second

INTRODUCTION

they dro orimarily manthatic or paraly functions to maintee commercial index, dates the wither and that that the specific of the shift or date manufal be at that the presiders. from a median within to manne with a same index to the main attraction to manne of shifts of the index to the test attraction to manne of shifts of the index to the test of sheater test along of a finestical index to the test of sheater with i mediance test index to the test of the sheater of the test of a index to the test of the sheater of the test of the index to the test of the sheater of the test of the index to the test of the sheater of the test of the index to the test of the sheater of the test of the index to the test of the sheater of the test of the index to the test of the sheater of the test of the index to the test of the test of the test of the sheater of the index to the test of the test of the test of the sheater of the index to the test of the test of the test of the sheater of the index test of the test of the test of the test of the sheater of the index test of the test of the test of the test of the sheater of the index test of the test of the test of the test of the sheater of the index test of the index test of the index test of the index test of the index test of test of the test of the test of the test of test of

As include the desired as a local sector.

There is no doubt that floodligthing a building is one of the most spectacular achievements in lighting engineering. A floodlit building is a focal point in a town, when it is dark and colours are blurred.

Formerly it was mostly buildings of historic interest that were floodlit. Floodlighting of these old buildings, which often boast rich, ornate facades and beautiful architecture, is still very effective. Such wonderful results can be achieved that often these buildings are reinvested in this way with some of their former glory.

The different uses to which floodlight is put, whether they are primarily aesthetic or purely functional to achieve commercial ends, does not alter the fact that the quality of the end product should be as high as possible. Even a modern office block with a bare frontage can be made attractive by means of artifical lighting. However, it must be said that, whatever the reason, it is better to abondon the idea of a floodlight installation than to be satisfied with a mediocre result.

Lighting engineer must follow four steps in application of lighting |

1- Determine the desired level of illumination
2- Select a luminare that will produce this level
3- Calculate the required number of luminaries

4- Lay out the installation for uniformity of illumination

Illumination can be divided into two groups as :

a) INDOOR ILLUMINATION

b) OUTDOOR ILLUMINATION

In this project Ulu Mosque is illuminated as an outdoor illumination.

In outdoor illumination there are two methods of calculation |

1- LUMEN METHOD

2- DIRECT METHOD

1- LUMEN METHOD | It can be said that it is a very practical method to determine the number of fittings. The number of fittings can be calculated by dividing the total flux to flux used of one fitting only.

2- DIRECT METHOD | By using this method and appliying the computer program including the intensity matrix, the illuminance at each point on the surface of the walls are obtained.

In this project lumen method is used to calculate the number of fittings.

DIVISION ILLUS ALLESSES A

A finality on the installectory provide can only be events one serversfully it a theorem is contract best as at the building operation. The institute sequences build contract further white best factors relating to institute homestication for the solutions to be even in the institute the state of a second of the factors upon it.

CHAPTER 1

terressioner elegizable profiles, arequires as a solute result

The approximate is the behavior of their is the training and the structure when the structure is believe a state of the structure is the structure is the structure is the structure of the structure is and any class of the structure of the struc

OUTDOOR ILLUMINATION :

I) PLANNING :

A floodlighting installation project can only be carried out succesfully if a thorough study has been made of the building concerned. The lighting engineer should become familiar with all factors relating to lighting installation for the building. It is essential he should first study the feature of the facade under various conditions and with the sunlight falling upon it at different angles in order to decide which are the most attractive features. If an on-the-spot survey is impossible, daylight photos, drawings or a scale model can be useful aids. An informative part of the daylight study is the analysis of how given effects arise.

The appearance of the building at night is therefore taken into account when designing the building and it is more important if this is the case, there should already be good cooperation, at this stage, between te lighting engineer and architect, in order to avoid any risk of architest's conception being misinterpreted. During the planning daylight plays very important role to decide the place of the fittings. If there is a cloudless sky and bright sunshine, two natural source of light can thus be said to be present at one and the same time. As a result of this condition hard shadows falling under projections on the facade and caused by direct sunlight are softened by the diffused light from the sky. Fundemantally, illumination by sunlight is the ideal form of floodlighting. Sunlight streaming down on a building causes shadows to form under facade projections on the side facing the viewer. The result is a never ending interplay of light and darkness on the facade, emphasizing the architectural features. For the ever available direct sunlight, the bas relief of the ancient Greek temples was already sufficient to create an interesting pattern of light and shadow on that type of sculpture. In Western Europe, however, with its often dull weather and cloudy diffuse sky, more relief was needed in the facades of the gothic cathedrals found there, in order to create the same interplay of light and shadow. This phenomenon reveals one of the first principles of floodlighting, which is that te direction of the light and the direction of view should be at an angle to one or other, preferably between 45 and 135.

THE CONTRAST BETWEEN THE FACADE AND THE BACKGROUND:

The contrast between the facade and its background changes continuously with changes in weather conditions. When, for example, the rays of the sun fall directly on the facade and there is a cloudless sky, the facade will be brighter than the background because of the grater reflection. Sunlight falling directly on the building causes hard shadows. When the sky is cloudless but the facade receives no direct rays from the sun the sky is brighter than the facade. The sky radiates light in all directions, while the facade merely reflects the light. Since the light is diffuse only soft shadows appear. If the sky is clouded over, diffuse light falls on the building. In such light a facade is less bright than the background, in that the light comes from the sky, moreover practically no shadows are seen. In practice, of course, all kinds of combinations of the cases, which have been considered above are possible.

It is not only the changing weather conditions and the varying contrasts between the facade and its background that are important in daylight studies, but also the changing aspects of the building over a given period of time. For example, during course of the day, the shadows move from one part of the facade to another owing the continuously changing position of the sun. Generally a building is at its best in the hours of the morning and just before sunset. This is because the sun is low in the sky at these times an we see the contrast in colour between the sunlight, which contains much red

light, and the diffused light from the sky, which contains great of blue.

It is possible to imagine that, in studying a building, the lighting expert may be attracted at a given moment by a certain striking effect and that this mental image sticks in his mind as the effect he would like to retain. This mental image is in many cases the initial point of departure of a floodlighting design. Proceeding from this mental image he must translate the natural lighting effect, which he has seen, into an artifical lighting effect. One of the first things to be noted is that at night the position of the light sources is completely different from the day time situation. Whereas the natural light sources illuminate the building from above, artifical light sources are generally placed low down near the building or a little higher on an adjacent building. Thus a clear idea of how the installation is to be carried out may be gained by methodically collecting all details relevant to te possible positions of light sources, the appropriate fittings and lamps, the reflecting properties of the surface material of the facade, the various points from which the building can be observed.

II) CARRYING OUT A FLOOLIGHTING PROJECT :

The following points should be considered when planning a floolight installation.

i) Direction of view : Decide on the main direction from which the building is wieved. Generally there will be several, but often one can be decided upon as the main direction of view.

ii) Distance : Decide on the normal distance between the viewer and the building, based on the main direction of view. Whether one can see all or none of the architectural details on the facade will depend on the distance chosen.

iii) Surroundings and background : Obtain a clear idea of the background against which the building will be see. If the surrounding and the back ground are dark a relatively small amount of light is needed to make the building lighter than the background. The colours of the light already present in the background of the building, even street lighting, must than be taken into consideration.

iv) Obstacles : Trees and fences around the building can form a decorative part of an installation. An attractive way of dealing with these is to place the sources of light behind them. Two advantages are gained :

1 - The light sources are not seen by viewer.

2 - The trees and fences are silhouetted against the light background of the facade. The impression of depth is therefore heightened.

v) Setting up the light sources : One of the most important points in designing a floodlight installation is to investigate all the possible ways of setting up the light sources. There many alternatives for mounting:
On street lamps or other posts specially erected for the purpose

- On the penthouse roof

- On brackets on te house front

- On the ground behind flower-beds, bushes or copses

If the building is located along a main road it must be borne in mind that te ligting must not hinder the traffic. Fitting should be well screened from the drivers of oncomings vehicles.

vi) The form of the building : Once the main direction of view has been chosen, the choice of direction of the light depends on the shape of a building or rather the form of its ground plan or horizontal section. The position of the light sources which are to cover the builing may then be more or less fixed. In theory it is possible to reduce all ground plans of buildings to

simple geometric figures ; square, rectangular or round. In the case of complex structures, the ground plan can be thought of as a group of such figures. For buildings with a square, rectangular or circular ground plan a basic lay-out exists which, in virtually all cases, leads to good results.

The characteristics of the facade show to best advantage when the incident light is at an angle smaller than 90. No definite angle can be given; on the horizontal and vertical planes the angle may vary between 0 and 90, calculating from the vertical to the facade. For deep profile the angle should be between 0 and 60, for a flat profile between 60 and 85 to the vertical.

III) ARCHITECTURE OF THE FACADE :

i) Flat facades : Flat facades without projections or architectural details do not lend themselves very well to floodlighting. Shadow effects may be achieved only when the light sources are placed very near to the facade. To prevent the result from being flat and uninteresting a certain unevenness in the brightness pattern should be created by the arrangement and adjustment of the floodlights.

ii) Facade with vertical lines : Vertical lines of a

facade may comprise pillars or supporting columns or, for instance, in modern glass facades the beams or girders carrying the floors. The vertical line of the wall can be emphasized by illumination from the left and right sides of the facade with medium-beam floodlights. In most cases the shadows produced in this way are too strong and create too marked a contrast, so that lighting from the opposite direction is needed to soften the whole shadow pattern. Wide-beam floodlights are therefore used, with the direction of the light parallel to the main direction of view must be such that the bands of shadow face the viewer.

iii) Facades with horizontal lines : Some facades have a decorative element, a horizontal band or slightly projecting beam. If in such cases the light fittings are placed too close to the facade. The result is a rather dark band of shadow above this projecting beam. This gives the impression that the building consist of two parts and that the upper part is floating in the air. To keep the band of shadow narrow there should be grater distance between the facade and the light fittings.

iv) Facades with projections : Projecting features such as balconies, penthouses, parapets or balustrades can add to the attraction of the facade if included in

the scheme. In this case the light fittings must be placed at some distance from the facade so as to prevent excessive shadow. If the site does not allow of this, supplementary lighting with small light sources may be mounted on projecting parts of the building.

v) Facades with recessed parts : These may be balconies which are set back or galleries with railings at the front. Obviously a large part of the built-in space will be in shadow if the floolights are placed only short distance from the facade. In such a case supplementary lighting will be required in the balcony and for this light of another colour may be used. If this is done, a particularly sitriking effect can be achieved, at the same time creating a greater impression of depth. Floodlighting from a larger distance, however, reduces shadow, making it less visible to the viewer, thus obviating the need for extra lighting.

vi) Mirror effects : Nearly every facade has a number of windows give a mirror effect especially when it is dark inside the builing. If, for instance, the floodlights are mounted on posts, the person viewing the building from below may be dazzled by the bright reflections from the ground-floor windows. This effect can be avoided by mounting light sources below eye level.

IV) SURFACE MATERIAL OF THE FACADE :

In determining the illumination level needed for a facade in order to obtain the required brightness, the reflection factor and the way the building surface material reflects the light are important factors to be borne in mind. The table below indicates the reflection factors of a number of different materials.

MATERIAL	STATE	REFLECTION FACTOR		
White marble Granite Light concrete Dark concrete Stone	fairly clean fairly clean fairly clean fairly clean very dirty	.60 .65 .10 .15 .10 .50 .25 .05 .10		
Imitation concrete paint	clean	.50		
White brick Yellow brick Red brick	clean new dirty	.80 .35 .05		

The total reflection from a facade depends on the following points :

- a) the material of the facade
- b) the incident angle of the light
- c) the position of the observer in relation to the reflecting material (specular reflections).
- d) the colour of the material (it is accentuated if light of the same colour is used).

A distinction can be made between diffuse reflection and specular reflection and of variations between the extremes. These different types of reflection are due to the particular surface textures of the different materials. Four classes may be distinguished :

1- Very smooth surface : A very smooth surface acts more or less as a mirror, with the result that most of the reflected light is directed upword, away from the observer.

2- Smooth surface : Light is reflected somewhat diffusely from a smooth surface; small amount of this light reaches the observer.

3- Dull surface : Incident light reflected from a dull surface is even more diffused, so that a larger part of the light is directed towards the viewer.

4- Very dull surface : Light reflected from a very dull surface is diffused to a large degree, an therefore a great part of the light is directed towards the observer. It is obvious that these different reflection properties of surface material necessitate a different illumination of the facade, in each case, in order to achieve the brightness. Even the mount of grime on a building is important; the reflection factor of a clean facade can sometimes be more than twice that of a grimy

facade. This was clearly illustrated recently when certain historic buildings were cleaned.

V) SHAPE OF ROOFS :

The appearence of a building at night is hardly complete if the roof, which is visible in the day time, is not visible when the building is floodlit. A flat roof is neither seen in the day time nor at night, and so lighting is restricted to the facade. In the case of a gable roof, however, the slope of the roof must be taken into account. If a building has a flat roof the top storey is often set back forming a gallery. The top storey can than be illuminated by setting the floodlight at a great distance from the facade. Alternatively the sharp - edged shadow can be softene by supplementary lighting using small light sources in the gallery itself. Another possibility is the use of light of a different colour in the gallery, which will then illuminate the whole of the top - storey facade.

VI) SELECTION OF THE LEVEL OF ILLUMINATION :

The lighting level needed on a facade to effect a certain brightness contrast depends upon such factors as the reflection factor of the surface building material, the location of the building in relation to its

surrounding and the dimensions of the building. The table below presents some recommended illumination levels for various surface building materials used on buildings in either poorly lit, well lit or brightly lit surroundings.

		illu	mination in	in lux		
TYPE OF SURFACE	STATE	P.L.S	W.L.S	B.L.S		
white marble	f.clean	25	50	100		
light concrete	f.clean	50	100	200		
imitation				100		
concrete paint	f.clean	100	250	400		
white brick	f.clean	20	40	80		
vellow brick	f.clean	50	100	200		
white granite	f.clean	150	300	600		
concrete	f.clean	75	150	300		
concrece	f clean	75	150	300		
red brick	vory dirty	reau	ires at lea	st		
concrete	distu	rega	150 - 300			
red brick	arrey		100 200			

P.L.S : poorly lit surrounding

W.L.S : well lit surrounding

B.L.S : brightly lit surrounding

SUPERCIPATE CRED IN COLUMNIAL

To Ministration protocta covers of areas and

the number outlided that five stronger and

the Managers source Achore come

1 - Par humbrid partners, autom such

3 - Kick pressure scales vehicle impo-

c - block peak may be party suggest 1. The

CHAPTER 2

and an endlars competitively.

DES PETRODAN ECCITOR VATOOR LAND I

The test this become conscient and the first the second and the test has been and the bound of a salve second and are lighting to apply of the same second and measure are spitter being that a good bigs reserves

- A Figh Unitabile -Statut
- A side of white limit
- · harancie: (obtain condition)
- · bene sennie to lite
- a polision, stable providence

EQUIPMENTS USED IN FLOODLIGHTING :

In illumination projects several types of armatures and lamps can be used.

Lamps can be devided into five groups as :

- 1 Low pressure sodium vapour lamps
- 2 Low pressure mercury vapour lamps
- 3 High pressure sodium vapour lamps
- 4 High pressure mercury vapour lamps
- 5 Metal halide lamps

In this project high pressure sodium vapour lamp (SON - T 250W, 100W, 70W) and HNF 003 are used as a lamp and an armature respectively.

HIGH PRESSURE SODIUM VAPOUR LAMP :

They are efficient, versatile light sources to start with their high luminous capacity means more light for less money and feature of often decesive importance where lighting is employed for a long periods of time.

Reasons are written below that why high pressure sodium vapour lamp is chosen to this project :

- * High luminous efficacy
- * Golden white light
- * Balanced colour rendering
- * Long economic life
- * Reliable, stable operation

- * Excellent lumen maintenance
- * Short re-ignition time

High-pressure sodium lamps combine very high efficacies (min.66 lm/W to max.130 lm/W) with moderate colour rendering, and are therefore suitable for many applications where such factors, together with good economics and long lamp life, are important. Experience has shown that, since the late sixties when SON lamps were introduced on to the market, these light sources have proved themselves particularly in terms of allround reliability. Compared with the version orginally launched, today's high pressure sodium lamps enjoy improved life, together with a higher light output and better lumen maintenance. On top of this, the brief reignition time (the time taken for the discharge to restrike should an interruption in the mains supply occur) represents an added safety feature; this interval is normally less than two minutes for lamps with an external ignitor in the circuit.

Structure of the SON lamp : The tungsten electrodes and their niobium supports are sealed into this tube with a specially developed cement to give a highly reliable seal. During this process, the sodium, mercury and a rare gas (xenon for SON and SON-T, and neon/argon for SON-H) to faciliate starting are also introduced

into the tube. Next, the tube is inserted into a clear, tubular envelope (SON-T) or built into an ovoid bulb with diffusing layer (SON). Here it is held in a place by the support wire. Extra protection is given by special support springs which cushion discharge tube against vibration. After these are fitted, the outer bulb is evacuated to minimise heat losses, a high vacuum being maintained by a getter which assists in ensuring maximum operating efficiency throught lifetime.

SON lamps in the range are ovoid types where the bulb wall has been electrostatically coated with a very uniform layer of calcium pyrophosphate. The use of this diffusing powder results in very low light losses and guaratees constantly high quality performance during the life of the lamp. Added to that, there is less glare so that simpler and less costly optical systems can be employed.

Like all gas-discharge lamps the SON lamps require a current limiting device, plus an ignitor to ensure rapid, reliable starting.

The initial discharge takes place in rare gas. Heat is thus dissipated, causing some of the mercury to evaporate. The sodium, with its lower excitation potential, then gradually takes over the discharge and after a short time the lamp burns stably, emitting its

characteristic, pleasant, golden - white light at luminious efficacies of up to 130 lm/W.

Some 80 % of nominal light output is reached within an average of four minutes. An additional advantage is the fast restrike time; for lamps with an external ignition device, this factor can be of the utmost importance in applications where short power suppl interruptions might otherwise lead to dangerous situations owing to lack of light (figures and wiring diagram about this lamp is given in the appendix).

HNF 003 (ARMATURE) :

This armature is the most convinient one for the SON lamps because of that it is used in this project. These are the descriptions about armature :

- Housing and rear cover of high pressure die-cast aluminium.

- Casting of low copper-content to excellent corrosion-resistance, even in coastal and industrial areas.

- High-grade aluminium reflectors for accurate beam control.

- Lamp replacement is effected by removing the rearcover, thus facilitating servicing.

- Easy to operate stainless steel clips on rear

cover; to be closed by hand and opened by using a simple tool.

- Cast-on beam-aiming sight and protactor scale for quick daylight adjustment.

- Silicone rubber gasket for jet proof and dust proof sealing of front glass.

- Front glass is a 5.5 mm. thick toughened glass plate, which is attached to the housing by 4 stainless steel clips, 2 extra safety brackets.

Applications : Sports grounds, floodlight of buildings, car parks, sport halls, shipyards (Details are given in the appendix).

1) UNITS AND DEFINITIONS USED IN ILLUMINATION :

LIGHT INTENSITY (I): Unit is called CANDELA and is 2 equal to 1/60 of the light intensity emitted by 1 cm of black body surface at the solidification temperature of platinium (2042 K). Light intensity is a vector quantity.

LIGHT FLUX (ϕ **) :** Unit is called LUMEN and is equal to the flux included in a solid angle of one steradian when the light intensity is 1cd in any direction.

ILLUMINANCE (E) : Unit is called LUX and is equal to 2 the flux falling on 1m of area. Sometimes "light level" is used instead of illuminance.

LUMINANCE (L): Unit is called NIT and is defined as light intensity emitted per unit area of light emitting surface.

REFLECTION FACTOR (n) : The reflection factors describes the relationship between the incident luminous flux and the reflected luminous flux. This factors depends upon the reflection properties of the surface of the material to be illuminated.

MAXIMUM INTENSITY (Imax) : The maximum intensity of the beam is the maximum intensity candela per 1000 lumen of the lamp flux.

II) METHODS OF CALCULATION :

There are two methods for calculating the types and numbers of floodlights needed to achieve the desired illumination; the lumen and direct (luminous intensity) method. For large facade lumen method and for high and small objects direct method should be used.

1 / LUMEN METHOD :

This method consists in calculating the number of lumens to be directed on to a facade in order to obtain a certain illumination level.

The number of lumens can be calculated by this formula :

$$\phi = \frac{A \times E}{n}$$

where : Ø : is the total number of lumens prodeced by all lamps,

- A : is the surface of the facade to be illuminated,
- E : is the desired illumination on that facade,
- n : is a factor which takes into account the efficiency of the fitting and the light losses.

The presence of a utilization factor in this formula

indicates that not all the lamp lumens contribute to the illumination level on the facade. The lumens produced by the lamps are concentrated by reflectors, inwhich process some loss is involved. If the initial output is 100 % lamp lumens, 60 to 75 % are projected through the lighting equipment and 40 to 25 % are lost fitting itself through interreflection in the reflector and absobtion by the other parts of the fitting.

After the floodlight has been in operation some time, a further percentage of the actual number of lamp lumens is lost because of the decrease in luminous flux due to the ageing of the lamp and dirt which collects on the lamp and fitting.

Finally a percentage of the losses is accounted for by wasted light, that is light not incident to the building facade. In this project utuilization factor is taken as 0.70. After finding the total luminous flux, the number of fittings (N) can be calculated easly as:

2 / DIRECT METHOD (LUMINOUS INTENSITY) :

In this method starting point is the luminous intensity, in candela, radiated by a light source in a

particular direction. This luminous intensity may be derived from the luminous intensity diagram or from a table. The calculation is made by this formula :

$$E = \frac{I}{h} \cos(x)$$

where; E : is the vertical illumination on the facade, I : is the luminous intensity at the angle (x), h : is the height of the object above the level on which the fittings are arranged,

x : is the angle at which the light beam strikes the normal on the plane to be illuminated.

CALCULATION OF THE PROJECT

BY USING LUMEN METHOD :Details about this method are given in the METHODS OF CALCULATION part of the project.These are the results of the calculations for each side of the building :

RIGHT HAND SIDE OF THE BUILDING :

width = 19.5 m height = 14.5 m area = 282.75 m Ø SON-T 250W = 27,000 lumen

2

2

 $\phi = 50 * 282.75 = 14,135.5$ lumen

 $\phi = 14,135.5 / 0.7 = 20,196.4$ lumen

N = 20,196.4 / 27,000 = 0.748 lamp

LEFT HAND SIDE OF THE BUILDING : width = 20.5 m height = 14.5 m area = 297.25 m Ø SON-T 100W = 10,000 lumen

 $\phi = 50 * 297.25 = 14,862.2$ lumen $\phi = 14,862.2 / 0.7 = 21,232.1$ lumen N = 21,232.1 / 10,000 = 2.1 lamps

FRONT & BACK SIDE OF THE BUILDING :

width = 36.5 m height = 14.5 m area = 529.25 m
Ø SON-T 250W = 27,000 lumen

 $\phi = 50 * 529.25 = 26,462.5$ lumen $\phi = 26,462.25 / 0.7 = 37,803.5$ lumen N = 37,803.5 / 27,000 = 1.4 lamp

TOWER : width = 5 m height = 23.5 m area = 117.5 m Ø SON-T 70W = 6,500 lumen

This lumen method is not an adequate method to calculate the number of fittings for such buildings. Because by using this method place of the projectors can not be found. This is a very important thing in floodlighting to know the place of the fittings. And also by using this method distribution of the illuminance on the wall of the building can not be calculated. So it is impossible to know illuminance at desired point of the building.

But direct (luminous) method gives all these requirements which are written above. So that in this project to illuminate this building direct method is used.

BY USING DIRECT (LUMINIOUS) METHOD :

Details about direct method is given in the METHODS OF CALCULATION part of the this project.

How to use direct method :These are the formulas to calculate C & GAMA angles.

$$B = Tan^{-1} \frac{\dot{X'} + \dot{Y'}o^{2}}{1 + \dot{Y'}o^{2}} - Tan^{-1} \frac{\dot{X'}o}{1 + \dot{Y'}o^{2}}$$

$$n = \frac{1 + Y' Y'_{0} + X'^{2}}{1 + Y' Y'_{0}} - \frac{1 + Y'_{0}^{2}}{1 + Y' Y'_{0}} - \frac{1 + Y'_{0}^{2}}{1 + Y' Y'_{0}} - \frac{1 + Y'_{0}^{2}}{1 + Y'_{0}^{2} + X'^{2}} \left[\frac{1 + Y'_{0}^{2}}{1 + Y' Y'_{0}}\right]^{2} \right]$$

$$Tan C = \frac{(Tan)}{Tan B}$$

$$Tan \mathcal{V} = (Tan^2 \beta) (1+Tan^2 \beta) + Tan^2 \beta$$

$$\cos^{3} \Theta = \frac{1}{(1+X'^{2}+Y'^{2})^{3/2}}$$

$$E = \frac{I_{c,\gamma}}{h^2} \cos^3 \theta$$

In the formulas :

Х	>	X '	,	Χ'	=	X/h
Y	>	Y'	,	Y'	I	Y / h
_X0	>	X0'	,	X0	=	X0 / h
YO	>	Y0 '	,	YO	=	Y0 / h

where : $\mathbf{X} \ \mathbf{\&} \ \mathbf{Y}$ represents the coordinates of the point at which the calculating of illuminance needed.

X0 & Y0 represents the coordinates of the surface of the point at which projector axis intercept the plane which will illuminate.

Results of the this formulas and computer program is given at the following pages. TOWER

Son Be say fa conpuder

brot Low

XO = O			Y0 = 5	h	=	4			
s	0	N	-	т	:	7 O W			

		(13)(3)	C	E
	¥ 	GAMA		
2	4	20.43	342.65	101.94
2	6	16.25	17.35	75.32
2	8	17.40	43.10	72.27
2	10	19.79	57.36	20.00
2	12	22.05	65.43	17.35
2	14	23.95	70.42	7.63
2	16	25.51	73.78	3.93
2	18	26.80	76.11	3.49
2	20	27.87	77.96	2.29
2	22	28.77	79.33	1.53
-2	4	20.43	197.34	101.94
-2	6	16.25	162.65	75.32
-2	8	17.40	136.86	72.27
-2	10	19.79	122.64	20.00
-2	12	22.05	114.57	17.35
-2	14	23.95	109.56	3.49
-2	16	25.51	106.22	7.63
-2	18	26.80	103.83	3.93
-2	20	27.87	102.04	2.29
-2	22	28.77	100.66	1.53
RIGHT-HAND SIDE OF THE BUILDING _____ _____ -----

-

X0 = 0 Y0 = 0 S O N - T : 250W

x	Y	GAMA	С	E	h
		7 59	0.00	65.30	15
2	0	14.90	0.00	51.90	15
6	0	21.80	0.00	39.45	15
8	0	28.07	0.00	27.60	15
10	0	3.69	0.00	15.80	15
-2	0	7.59	0.00	65.30	15
-4	0	14.90	0.00	51.90	15
-6	0	21.80	0.00	39.45	15
2	-2	8.04	315	110.60	20
4	-2	12.60	333.45	76.85	20
6	-2	17.54	341.56	67.16	20
8	-2	22.40	345.96	75.87	20
-2	-2	8.04	225.00	110.60	20
-4	-2	12.26	206.56	76.85	20
-6	-2	17.54	198.43	67.16	20
2	-4	10.14	296.56	46.41	25
4	-4	15.79	315.00	91.38	20
6	-4	16.08	326.30	63.95	30
-2	-4	11.49	243.43	127.91	22
-4	-4	14.42	225.00	76.50	22

X Y		GAMA	С	E	h
-6	-4	18.14	213.69	77.18	22
2	-6	14.19	288.43	136.50	25
4	-6	16.08	303.69	55.00	25
6	-6	18.74	315.00	54.09	25
-2	-6	14.19	251.56	136.50	25
-4	-6	35.79	236.30	126.30	10
-6	-6	40.31	225.00	48.71	10
2	-8	13.20	284.03	31.60	35
4	-8	14.30	296.56	48.70	35
6	-8	15.94	306.80	45.04	35
-2	-8	28.79	255.96	92.61	15
-4	-8	30.80	243.43	58.30	15
-6	-8	33.69	233.10	47.80	15
2	-10	18.77	281.30	28.40	30
4	-10	19.74	291.80	25.18	30
6	-10	21.24	300.96	24.97	30
2	10	34.21	78.69	32.19	15
4	10	35.67	68.19	32.20	15
6	10	37.86	59.03	26.30	15
-2	0	7.59	0.00	65.30	15
-4	0	14.90	0.00	51.90	15
-6	0	21.80	0.00	39.45	15
2	2	8.41	45.00	110.60	20
4	2	12.60	26.56	76.85	20

X Y		GAMA	С	E	h 		
		17 54	18.43	67.16	20		
0	2	22.40	14.03	75.87	20		
-2	2	8.04	135.00	110.60	20		
-4	2	12.26	153.43	76.85	20		
-6	2	17.54	161.56	67.16	20		
2	4	10.14	63.43	46.41	25		
4	4	15.79	45.00	91.38	20		
6	4	19.82	33.69	63.95	30		
-2	4	11.49	116.56	127.91	22		
-4	4	14.42	135.00	76.50	22		
-6	4	18.14	146.30	77.18	22		
2	6	14.19	71.56	136.50	25		
4	6	16.08	56.30	55.00	25		
6	6	18.74	45.00	54.09	25		
-2	6	14.19	108.43	136.50	25		
-4	6	35.79	123.69	126.30	10		
-6	6	40.31	135.00	48.71	10		
2	8	13.20	75.96	31.60	35		
4	8	14.30	63.43	48.70	35		
6	8	15.94	53.13	45.04	35		
-2	8	28.79	104.03	92.61	15		
-4	8	30.80	116.56	58.30	15		
-6	8	33.69	126.86	47.80	15		
2	10	18.77	78.69	28.40	30		

x	Y	GAMA	с	E	h
4	10	19.74	68.19	25.18	30
6	10	21.24	59.06	24.97	30
2	-10	34.21	281.30	32.19	15
4	-10	35.67	291.18	32.20	15
6	-10	37.86	300.96	26.30	15

L	E	F	т	-	Η	A	N	D	S	I	D	Е	0	F	Т	H	E	В	U	I	L	D	I	N	G

X0 = 5 Y0 = 6 S O N - T = 100W

x	Y	GAMA	С	E	h		
0	2	34.47	223.20	104.50	8		
0	4	28.30	202.10	88.80	8		
0	6	26.56	00.00	28.01	8		
0	8	27.69	162.29	115.20	8		
0	10	29.90	150.00	13.67	8		
0	12	32.49	141.80	53.62	8		
2	0	36.60	257.30	122.09	8		
4	0	30.60	275.59	89.80	9		
6	0	30.50	294.70	65.40	9		
2	2	24.97	243.20	108.10	8		
2	4	16.20	216.30	147.20	9		
2	6	15.25	00.00	36.20	8		
2	8	18.23	152.45	82.40	9		
2	10	22.30	139.60	16.40	8		
2	12	25.30	130.00	10.80	9		
4	2	20.40	93.20	105.80	8		
4	4	9.60	257.40	96.80	8		
4	6	4.76	00.00	37.50	8		
4	8	10.30	131.90	50.16	8		

х	Y	GAMA	С	E	h
4	10	15.70	119.00	37.46	9
4	12	20.74	114.80	30.84	9
6	2	21.61	301.58	79.38	8
6	4	7.58	302.30	41.40	15
6	6	3.17	00.00	17.54	15
6	8	7.35	77.39	53.72	8
6	10	13.09	93.20	72.70	8
6	12	18.10	96.50	26.02	8
8	3	15.80	320.00	16.60	13
8	5	11.14	343.00	39.90	13
8	7	9.74	18.70	29.20	13
8	10	13.50	57.90	26.30	13
8	12	17.39	70.00	9.87	13
10	3	20.40	332.00	23.92	13
10	5	15.40	349.20	22.09	15
10	7	15.10	11.30	22.11	13
10	9	15.09	32.10	77.15	15
10	11	17.29	47.70	18.25	15
10	13	20.00	58.40	13.82	15
12	3	24.80	338.80	17.66	13
12	5	21.73	352.30	19.10	13
12	7	20.08	7.99	16.08	13
12	9	19.90	23.80	14.15	13

x	Y	GAMA	С	E	n
10	11	20.97	37.50	15.71	13
12	13	22.70	48.50	12.57	13
14	10	23.89	24.60	15.60	13
14	12	24.60	35.40	9.30	13

ROAT & CREE FOR BE SEA BUILDING BRIDGE PART OF THE BUILDING

$$X0 = 5$$
 $Y0 = 0$ $h = 5$

-

S O N - T = 70W

x	У	GAMA	С	E
1	0	33.69	00.00	56.23
2	0	23.19	00.00	83.53
4	0	6.34	00.00	71.45
2	5	47.65	113.00	39.84
4	5	38.43	98.05	24.39
5.5	5.2	35.06	86.11	17.24
2	-5	47.65	113.00	39.84
4	-5	38.43	98.05	24.39
5.5	-5.2	35.06	86.11	17.24

FR	ONT	3	В	A	C	K	S	I	D	E	0	F	т	H	E	В	U	T	ц	D	+	T.	9
----	-----	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	----	---

X0 = 1 Y0 = 0 S O N - T = 250W

x	Y	GAMA	С	E	h
0	2	5.11	116.55	50.40	25
0	4	9.37	104.03	83.50	25
0	6	16.93	99.97	70.80	20
0	8	21.97	97.13	61.40	20
2	0	2.84	00.00	39.80	20
4	0	8.44	00.00	35.56	20
6	0	13.80	00.00	29.15	20
-2	0	11.40	00.00	61.50	15
-4	0	18.70	00.00	47.28	15
-6	0	25.60	00.00	35.01	15
2	-2	5.78	296.50	137.60	22
4	-2	9.23	326.80	101.07	22
6	-2	12.04	338.10	121.60	25
2	-4	10.58	284.00	80.80	22
4	-4	12.70	306.80	118.00	22
6	-4	16.00	321.30	48.60	22
2	6	15.40	80.54	58.60	22
2	8	20.06	82.89	46.62	22

х	Y	GAMA	С	E	h 		
4	2	9.23	34.00	101.01	22		
4	4	12.71	53.20	118.03	22		
4	8	21.08	69.50	45.30	22		
6	6	19.33	50.23	22.74	22		
6	8	22.08	58.02	41.42	23		
8	8	25.43	48.85	32.71	22		
-2	-2	14.59	146.25	124.30	14		
-2	-4	19.80	126.80	114.90	14		
-2	-6	25.87	116.61	100.80	14		
-4	-2	20.08	150.26	89.40	15		
-4	-4	25.04	141.37	89.60	14		
-4	-8	34.57	128.00	43.62	14		
-4	-10	39.24	116.50	32.54	14		
0	-2	5.11	116.65	50.40	25		
0	-4	9.37	104.00	83.50	25		
0	-6	16.93	119.46	70.80	20		
0	-8	21.97	97.12	61.40	20		
2	2	5.78	63.45	137.60	22		
4	2	9.23	33.20	101.07	22		
6	2	12.04	21.90	121.60	25		
6	4	16.00	38.70	48.60	22		
-2	2	14.59	146.25	124.30	14		
-2	4	19.80	126.80	114.90	14		
-2	6	25.87	116.51	100.80	14		

x	¥	GAMA	С	E	h
-4	2	20.08	158.16	89.40	15
-4	4	25.04	141.28	89.60	14
-4	8	34.57	121.94	43.62	14
-4	10	39.24	116.51	32.54	14

DIMENSIONS :

XO, YO, X, Y, h = meter

GAMA, C = degree

E = lux

COMPUTER PROGRAM FOR DIRECT ILLUMINATION

	DIMENSION OGA(37 REAL E,X,h,GAMA, REAL C3,T,R,O,O1 OPEN(1,FILE='MAT DO 10 I=1,37 DO 10 J=1,19	.37) X0,Y0,X1 ,02,T1,I RIX')	,Y1,C,B,B NT,PR1,PR	1, B2, BETA 2, R1, R2	
10	READ(1.*)OGA(I,J CONTINUE CLOSE(1) DO 20 I=1,37)			
20	DO 20 J=1,18 OGA(I,19+J)=OGA(WRITE(*.*)'PLS, READ(*.*)X0.Y0	I,19-J) ENTER X(),YO POINT	S'	
	WRITE (*.*) 'PLS, READ (*.*) h OPEN (2, FILE='OUT WRITE (5,9) X0, YO WPITE (2,9) X0, YO	ENTER DI	ISTANCE '		
9	FORMAT($6X$, ' $XO=$ ',	F6.4,4X	,'YO=',F6. v	4,5X,) GAMA	С
\$	WRITE(3,*)' E h ' WRITE(2,*)'	A	v	GAMA	- -
\$	$\frac{\text{WRITE}(2, *)}{\text{E}}$	Λ	I	GAMA	Ŭ
19	WRITE(2,19) FORMAT(7X,60('-' OPEN(1,FILE='F77	')) 7')			
5	WRITE(*.*)' PLS, READ(*.*) X,Y X1=X/h Y1=Y/h X01=X0/h Y01=Y0/h	, ENTER 3	X,Y POINTS	; 1	
	B1=ATAN ((X1*SQR B2=ATAN (X01/SQR B=B1-B2	F(1+Y01* F(1+Y01* *Y01)+(Y	YO1)/(1+Y1 YO1)) 1*Y1(1+YO1	*YO1))	*V01)))
\$ \$	/ SQRT((1+X1*X1- /(1+Y*Y0)(1+Y*Y0) C=ATAN(TAN(BETA)	+Y1*Y1)()))) SQRT(((YO1*YO1+XC TAN(B)*TAN	(B) + 1) / (TAN (B) + 1) / (TAN (BFTA))) * (1+)	V(B))))
\$	(B))*(TAN(SQR1((B))*(TAN(B))) C3=1/((1+(X1*X1 C=(C*180)/3.141) GAMA=(GAMA*180) IF((X.LE.0).AND	((IAN(BE))+((TAN(B))+(Y1*Y1)) 5926 /3.14159 .(Y.GE.0)	(TAN(B)) * (TAN(B))) * * (1.5)) (126) $C=180+0$		((

```
IF((X.LE.0).AND.(Y.LE.0)) C=180-C
IF((X.GE.0).AND.(Y.LE.0)) C=360-C
I=GAMA/2.5+1
J=C/10+1
IF (MOD(0,10).NE.0) THEN
T = OGA(I, J)
R=OGA(I, J+1)
01=10*(R-0)/(R-T)+T
T = OGA(I+1, J)
R=OGA(I+1,J+1)
02=10*(R-0)/(R-T)+T
T1 = OGA(I, J)
INT=T1-2.5*(GAMA-T1)/(02-01)
ELSEIF (MOD (GAMA, 2.5).NE.0) THEN
PR1=OGA(I,J)
PR2=OGA(I, J+1)
R1=2.5*(PR2-GAMA)/(PR2-PR1)+PR1
PR1=OGA(I+1,J)
PR2=OGA(I+1,J+1)
R2=2.5*(PR2-GAMA)/(PR2-PR1)+PR1
01=OGA(I,J)
INT=01-10*(0-01)/(R2-R1)
ELSE
INT=OGA(I,J)
ENDIF
E = (INT * 10 * C3) / (h * h)
WRITE(5,80)X,Y,GAMA,C,E,h
WRITE(2,80)X,Y,GAMA,C,E,h
FORMAT(6F10.3)
GOTO 5
CLOSE(1)
END
```

CHAPTER 3























SCALE 1:50 BRIDGE PART

1/17 Ales





COST OF THE PROJECT

MATERIAL	UNIT PRICE	PRICE
Main distribution table.(circuit breaker 60A, fuses 13A)	1,350,000.	1,350,000.
Timer (kWh meter)	600,000.	600,000.
2 2 2*6mm + 1*1mm PVC cable	100,000.	1,500,000.
2 2 2*16mm + 1*1mm PVC cable	140,000.	1,400,000.
250W projector+armature	2,100,000.	10,500,000.
100W projector+armature	1,800,000.	3,600,000.
70W projector+armature	1,500,000.	7,500,000.
Cost of the labor %40 of	material cost	: 15,980,000.

(Prices are given in TL) 55,930,000.

DISCUSSION & CONCLUSION

Floodlighting is the lighting, usually by projection of the whole of a scene or object to a level considerably grater than that of its surroundings. There are some factors that floodlighting engineer should be very careful in order to get good results. For example, average illuminance, choice of light sources, coefficient of regularity, number of armatures and so on. According to convenient choosing of these factors, project can be successful or not. Because, in designing an installation of floodlighting for a building, the all important consideration is the final appearence of the building as whole as seen by the majority of the observers. The project must be to make picture which will have the right impact on the passer by.

In this project by considering all these features (which are written above) I tried to get beauties of this building to reveal by night as well as by day.

Aim of this project to improve my knowledge about the outdoor illumination by using educational studies. During this project I have seen that what floodlighting is in practical life, and also I catched the chance to use my imagination while illuminating this building. Also during the calculation part of this project I have

seen that lumen method is not an adequate method to do such a project. So that I used direct method as well as lumen method to get more accurate and acceptable results in this project.

APPENDIX

an entering of the relation the basic first function of

and the second se

Type of base			Luminous	Average lamp	Average lamp	Run-up time	Burning position	Bulb shape	
ittage	E27	B22	E40/45	Im	voltage V ¹¹	current A"	min. ²¹		
						1.0	٨	-	
50	2x 87s			11250	90	1,0	4	(Y-))	DA
SO	2x FC2			20000	100	3,0	4	45.	
70	2x 175			5000	95	1,0	4	-	
									15 Average
		. 81		4500	68	0,62	7	(T)	
35		.61		7400	107	0,59	7	110.	STATE TO A
55		•		1400		0.00	0		- share to and a share
90		,61		13000	117	0,83	10		
125		. 81		21500	176	0,82	10	City P	I SALASSING AND
180		. 6)		33000	250	0,83	12		
1.0		.6)		1800	57	0,35	11		
10		•(3)		3500	83	0,35	15	110.	
36		• 61		5700	114	0,35	13	SP	
	an in the data of the second se	.6)	a destances apply - a start confiden	10700	115	0,62	15		
00		• 61		17500	165	0,62	15	20.	and a specific of
131		•61		26000	245	0,62	15		
50				3300	85	0,76	5		- Charles
30				5600	90	1,0	5		Carrow Carrow State
100	•			9500	100	1,2	5	\cap	
100				13500	100	1,8	5	(.)Any	THE ,
150				15500	100	1,8	4		
150				25000	100	3,0	5.	-	A Prove Station
250				47000	105	4,4	5		- 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1
400			. 31	120000	110	10,3	6		
1000							E		
50				4000	86	0,75	5		
70				6500	86	1,0	5		- Stern her
100				10000	100	1,2	5	\cap	
150				14000	100	1,8	C	(.)Any	
150			•	16000	100	1,8	4	. ()	
250				27000	100	3,0	5	-	
400			•	47000	100	4,6	3		C TELE - SHE
1000			• 3)	125000	100	10,6	0		
				18000	104	2.5	3		V GUITT
210			•	24500	117	3.6	3	()	- march
350			•	34300	11/	0,0		\smile	

15-14-16

0 burning hours. mber of minutes after which the lamp has reached 80 ··er cent of its final luminous flux. x 50. amps are connected directly to the mains. The data given in this table refer to the 220-230V version. mended burning position, especially when undervoltage is expected.

PHILIPS | IGHIFNG B.V. | Computer Aided Lighting Design Lighting Design and Engineering Centre | DATABASE 2.00 Spring 1930 Computer Aided Lighting Design | Philips Lighting B.V.

Luminaire (INR) number	2.0	73			
Measuring code Luminaire type Lamp type		LVO 4147 HNF 003-W SONT 400W			
Lamp flux No. of lamps per luminaire Power dissipation	***	47.00 1 431.00	k∟ume Watt	n	
Total light output ratio Downward light output ratio	6 H 2 D	67 67	% %		
SLI-factor (Road lighting)	•	0.00			
Maximum spacing/height ratio	6	Lengthwise *	Cross *	Wise	
Luminaire sizes [mm]	4 8	Length O	Width O		Н0 0
Symmetry code	:	4			
CIF Fluxcode [%]		N1 N2 82 99	N 3 100	N4 100	

Н<u>а</u>р 0 PHILIPS LIGHTING B.V. | Computer Aided Lighting Design Lighting Design and Engineering Centre | DATABASE 2.00 Spring 1990 Computer Aided Lighting Design | Philips Lighting B.V.

Luminaire (INR) number	: 73
Measuring code	: LVG 4147
Lumination type	: HNF 003-W
Lamp typ.	: SCOFT 400W

* T-Table *

	0.0	10.0	20.0	30.0	40.0	,50.0.	60.0	70.0	80.0	0.00	100.0
	+	and and and on the se	- and also also also also also		an tain samp open when they be	r narr i na hais hàise narr na	. 1994 1995 1994 1996 199	in any op will with both bills	gana nav nava tanır bur nav	> C;	plen
0.0	1 810	612	610	612	612	612	612	612	612	612	612
0,0 -2 R	1 602	590	600	601	602	603	604	606	608	610	600
6 0	I BAR	526	688	589	590	587	589	589	592	5.97	592
7 5	1 5.64	565	SFR	565	564	566	569	574	577	583	577
10 0	1 620	6.20	633	253	529	546	556	567	574	583	574
10.0	1 500	507	502	610	615	526	549	572	585	597	585
15 0	1 200	1.08	4.20	1.77	1.20	520	54.8	572	587	597	586
43 6	1 1.52	407	1.50	150	1.71	511	577	552	560	556	560
20.0	1 400	126	423	427	462	496	507	503	507	510	507
20.0	1 107	401	200	410	444	466	456	456	457	455	457
25 0	1 279	303	381	402	416	417	414	408	399	400	329
27 5	1 3/13	350	395	387	3.9.9	381	376	363	346	341	348.
10 0	1 303	306	324	359	362	344	336	2164	293	287	20-
14 5	1 257	264	2.9.2	325	323	308	290	214.	248	. 234.	24
35.0	1 211	221	254	285	297	273	252	233	206	196	206
37 5	1 164	178	214	237	246	233	217	201-	181	179	18:
40.0	1 122	133	168	194	206	196	182	175-	171	163	171
42.5	1 86	9.9	127	153	170	166	154	153	151	1/17	151
45.0	58	6.9	3.9	119	139	141	134	130	129	135	100
47.5	1 45	4.9	63	90	113	110	113	116	108	110	101
50.0	1 32	37	40	70	91	9.9	9.8	92	37	90	13/
52.5	20	25	3.5	5.6	7.0	82	100	45	66	6.9	ЬĘ
55.0	1 12	16	21)	41	49	6.8	72	10	45	3.7	45
57.5	9	10	10	21	3.3	44	2.1	0	22	1.9	21
50.0	6	8	7	10	13	12	7	7	11	5	11
92.5	1	5	15	5	3	3	5	1	4	5	4
45.0	2	3	4	2	3	3	5	7	2	6	12
67.5	2	3	.3	3	2	2	4	6	7	5	
20.0	1	.?	2	2	, 2	- 2	11	6	6	5	
12.5	1	1	2	2	1	2	3	5	6	5	f5
75.0	1	1	1	1	1	2	3	4	5	3	5
77.5	1	1	1	1	1	. 1	2	3	λę.	2	4
80.0	1-	0	0	-0	ł	1	1	2	2	1	12
82.5	0	0	. ()	0	0	n	1		1	0	1
85.0	()	()	0	n	0	0	0	0	0	0	Ū
87.5	()	Ū.	{]	0	0	0	0	0	0	0	0
90.0	0	ŧ)	U	0	0	0	0	0	0	0	0

V Gamma-angle

and when many first they many when the too the state and the state and the state state state and the HILIPS LIGHTING B.V. | Computer Aided Lighting Design ighting besign and Engineering Centre | DATABASE 2.00 Spring 1990 Smputer Aided Lighting Design | Philips Lighting B.V.

iminaire (INR) number : 73

easuring code	: LVO 4147
iminaire type	: HNF 003-W
amp type	I SONT 400W

I-Table *

110.0 120.0 130.0 140.0 150.0 160.0 170.0 180.0 190.0 200.0 210.0 the test test and any set of the and the test set 0.0 1 612 / 612 2.5 5.0 7.5 0.0 12.5 15.0 0.0 503 457 . 450 503. -426 426 22.5 25.0 4.17 27.5 0.0 12.5 | 274 .325 5.0 17.5 0.0 12.5 5.0 8.9 7.5 0.0 2.5 5.0 0.0 th. 2.5 S 5.0 | Э 4 2 3 2 3 2 2 1 0.0 2.5 | 5.0 | 7.5 | i 1. 0.0 | 2.5 () D. 5.0 | () () O. n. 7.5

mma-angle

0.0

()

()

()

()

··· 14 ··· Date : 1998/08/07 | Computer Aided Lighting Design ILIPS LIGHTING B.V. anting Design and Engineering Centre | DATABASE 2.00 Spring 1990 nputer Aided Lighting Design | Philips Lighting B.V. and the set was been as an an an an an an

a

PHILIP Lighti Comput	S LIGHT ng Des er Alde	FING B Ign an ed LTgl	V. d Engi nting (ncerin Design	g Cent		Sompute DATABA Philips	er Aid de 2. s Ligh	ed Lig 00 ting B	hting (Spring V.	ສະເຊີຊະນ ວິຊາງໂຕຍນ 1990
									a and and and		
Lumina	ire (li	IR) nur	nher		: :3						
Mensur	ing cod	12			: 1.970	h 1 h 2					
Lumina	ire typ) ()			HNG	003 W					
Lamp t	Y P +				: SOM	400₩					
8											
* I-TA	ble "										
	200 0	000	0100								
	220.0		2411.0	250.0	260.0	270.0	200.0	290.0	300.0	310.0	32010
	1									C	-prane
0.0	612	612	612	612	612	612	612	612	612	512	612
2.0	602 EDG	603	504	606	608	610	608	606	50h	603	6.0.2
7 5	1 550	537	589	589	592	5.37	592	589	589	5.9.7	594)
10.0	530	546	SOS	574	511	583	577	574	569	566	they for the
12.5	515	526	549	573	525	0.00	574	570	555	546	539
15.0	4.89	520	548	572	586	597	586	670	543	0.00	513
17.5	1 471	511	507	552	550	568	560	552	537	511	4.7.1
-20.0	4.62	498	507	503	507	510	507	500	507	4.96	4.62
22.5	4114	456	456	456	457	458	457	456	456	466	444
25.0	416	417	414	408	399	400	399	408	15 1 /4	417	416
27.0	1 382	381	376	063	346	341	346	363	376	3.8.1	388
20.0	1 302	344	330	316	293	287	293	316	036	3 4 11	362
35.0	1 287	273	200	214	248	239	248	214	290	308	323
37.5	245	233	217	201	181	170	1.9.1	233	202	2/3	31
40.0	206	196	182	175	171	163	171	175	182	196	206
42.5	170	168	154	153	151	146	151	153	154	166	170
45 0	139	141	134	130	129	130	129	130	134	141	139
47.5	113	118	113	116	108	111	109	116	113	118	113
50.0	91	9.9	98	92	87	90	137	92	9.8	9.9	91
54.5	1 70	60	100	45	66	69	66	45	100	8.2	2.0
57.5	1 23	00 11 li	21	10	45	43	45	10	12	15.8	119
80.0	13	12	~ 7	.) 7	11	12	14	21	21	12	2.2
62.5	3	3	5	7	- 4	5	11	~	1	ية ا د	1.3
65.0	3	3	5	7	2	5	2	7	5	3	2
67.5	2	2	L	6	7	6	7	6	h	2	2
70.0	2	2	4	6	6	5	6	6	11	2	5
72.5	1	2	3	5	6	5	6	5	3	2	1
70.0		2	3	4	5	i,	5	1	3	2	1
80.0		1	2	3	4		4	3	0	1	ž
82.5	1 0	0	1	1	et. J	1	2	2	1	1	1
85.0	0	0	0	0	1	0	1	1	1	0	(1
87.5	0)	0	0	0	0	0	0	0	U	1
90.0	1)	0	0	0	0	0	0	0	. 0	11	11

v Gamma-angle

10

 PHILIPS LIGHTING B.V.
 | Computer Aided Lighting Design

 Lighting besign and Engineering Centre
 | DATABASE 2.00
 Spring 1999

 Computer Aided Lighting Design
 | Philips Lighting B.V.

C-plane

fuminairs (1012) number

Measuring code Luminaire type Lamp type

: LVC 4147 : HNE 003-W : SONI 400W

* I Table !

V Gamma-angle

HILIPS

NITION

light for one of the folg lamps: 400 W metal halide lamp

400 W mercury vapour

T 250 W or 400 W highure sodium lamp.



LIGHTING CATALOGUE

RIPTION

using and rear cover of high-pressure die-cast aluminium stings of low copper-content for excellent corrosion-istance, even in coastal and industrial areas. o beam-versions, as different reflectors are available:

HP1/T 400 W and

	HP/T 400 W	SON/T 250 W	SON/T 400 W
v beam:	2 x 7°	2 x 7°	2 x 7°
beam:	2 x 27°	2 x 27°	2 x 27°

h-grade aluminium reflectors for accurate beam control np replacement is effected by removing the rear-cover, thus ilitating servicing

sy-to-operate stainless steel clips on rear-cover; to be closed hand and opened by using a simple tool.

e floodlight cannot be easily opened by unauthorized per-IS.

RING DATA

Cast	on beam-aiming	sight	and	protractor	scale	for	quick	day-
light	adjustment.							

- Silicone rubber gasket for jetproof and dustproof sealing of front glass.
- The front glass is a 5,5 mm-thick toughened glass plate, which is attached to the housing by 4 stainless steel clips; two extra safety brackets.

APPLICATIONS

- Sports grounds Floodlight of buildings
- Marshalling yards
- Car parks
- Skating rinks _
- High-mast lighting
- Sports halls Shipyards

		Ordering number *		Weight
Designation	For lamps	Narrow-beam type	Wide-beam type	kg
	1 x SON/T 250 W	9112 702 302	9112 702 303	7,30
HNF 003	1 x HP/T 400 W	9112 702 426	9112 702 427.	7,30
	1 x SON/T 400 W or	9112 702 448	9112 702 449	7,30

Complete floodlight



FLOODLIGHT FOR METAL HALIDE LAMP, MERCURY VAPOUR LAMP OR HIGH-PRESSURE SODIUM LAMPS

きを
INF 003 - XNF 003 G

1	192	SIIIC	auc	11	
-				-	-
		Å.	~	~	

°55 ₩ /

HNF 003 and XNF 003 G loodlights for : High-pressure sodium lamps

x SON-T 250 W x SON-T 400 W	: HNF 003	
Metal halide lamps	5	
x HPI-T 400 W	: HNF 003	
ow-pressure sod	ium lamps	
x SOX 35 W	: XNF 003 G	

General description of the HNF 003 and INF 003G floodlights

xceptionally good photometrical erformance, excellent hechanical construction and easy haintenance characterise INF 003/XNF 003G floodlights. A choice of lamp types in various heam widths are available. The HNF 003 is suitable for a great humber of different floodlighting projects, such as:

- Sports facilities: sports grounds, sports halls, skating rinks,
- Traffic areas: marshalling yards, shipyards, car parks, high-mast traffic junction lighting,
- Floodlighting of buildings.
- required, the HNF 003 floodlights

can be equipped with a mattblack anodized sheet-aluminium louvre, to screen the lamps from direct view and thus limit glare. The XNF 003G floodlight, with built-in gear for 1 SOX 35W lamp is used for rather confined areas, such as smaller marshalling yards and shipyards, for fence lighting and other security lighting objects. The floodlights have a cast-on beam-aiming sight and protractor scale for quick daylight adjustment.

Lamp replacement is effected by removing the rear cover, thus facilitating servicing.

Materials

- Housing and rear cover of high-

pressure die-cast aluminium.

- The front glass is a 5 mm thick toughened glass plate, which is attached to the housing by four stainless steel clips.
- High-grade aluminium reflectors for accurate beam control.
- Castings of low copper-content for excellent corrosionresistance, even in coastal and industrial areas.
- Easy-to-operate stainless-steel clips on rear cover; to be closed by hand and opened by using a simple tool. The floodlight cannot be easily opened by unauthorized persons.
- One PG 11 gland for cable entry.
- Silicone rubber gaskets for jetproof and dustproof sealing of the front glass and rear housing.

RAWING

ass clips (4x)

ass c reflector lector

rear cover Ider bracket lder ver flector clip top (2 x) al block entry upport | clip bottom (2 x) bracket (2 x)



REPLACEMENT OF FRONT GLASS

Remove the two safety brackets
 Open the four clips by placing a screwdriver in the appropriate holes

ADJUSTMENT POSSIBILITIES

DIMENSIONS





HIGH PRESSURE SODIUM (SON)

SOLARCOLOUR

Solarcolour lamps are available in four shapes each with its own function, for use in The most extensive range of high pressure sodium lamps available from one manufacturer.

specialised luminaires.

There are two colours (Standard and De Luxe). De Luxe for areas where better colour rendering is required, e.g. offices and shops etc.

The unique Plus range now not only offers between 10 to 20% more light than its standard equivalent, but maintains its light output better, and in addition Plus lamps last longer.



	. 2									SO			220-250	310-430	500	1000			-0							
	Lighting Design Lurnens 2000 hrs	10000	15250	22500	27600	35500	41500	48000	65000	139000		15250	27000	48.000	70000	127000		3:00	5500	10000	14500	21500	00092 -	3450C	40000	
	Initial Lumens 100 hrs	10500	16000	24000	28600	37000	43500-	50000	700:00	135000		16000	28000	A Subject	74000	132000		3500 -	6000	10500	15250	23000	27000	36000	42000	
			ų			@ 310W	@ 360VV				ut starter]						starter)							@ 310W	@ 360VV	
3	Std Pack	10	01-	10	10	10		01	01	4	(witho	10	10	10	10	10	(with s	40	40	10	97	-10	- 10	10		
	Cap	E27 (ES)	E40 (GES) .	E40 (GES)	E40 (GES)	E40 (GES)		E40 (GES)	E40 (GES)	E40 (GES)	T E	E40 (GES)	E40 (GES)	E40 (GESI	E40 (GES)	E40 (GES)	ON-E A	E27 (ESI	E27 (ES)	E27 (ES)	E40 (GES)	-E40 (GES)	E40 IGESI	E40 (GES)		
	Ainimum Nominal Supply Volts	220	220	220	· C22	220	230	220	380	360	ılar SON-	220	220	220	220	220	iffused S	220	220	.220	220	220	220	220	230	
	Watts	120	150	220	250	313/360		400	609	:000	Clear Tubu	150	250	37	2020	000:	Elliptical D	50	70	120	:50	220	- 250-	310/360 -		

I-T, SONP-T,

SONDL-T

0 222123

0 (1)

10/

4

000000

50 864 50 864 50 864

(I)

Elliptical Diffused SON-E /E/ [without starter]

14500	26000	46500	
15250	27000	43500	
10	. 01	10	
 E40 (GES)	E40 (GES)	E40 (GES)	
220	220	-220	
150	250	100	-

U

ഹ

<۲

SON-E, SONP-E.

T m l

36000 42000 43500

46500

000

E40 (GES) E40 (GES)

400

220 230 220

SONDL-E

 $\sqrt{\Lambda}$ This international symbol which is marked on all Solarcolour lamps which have an internal snap states switch, indicate that they can be used in luminaires whether or not they have an external statter ----

E Lamps marked with this symbol can only be used in luminaries fitted with an external starter.

Manufactured to IEC662.

fitted.

For further technical information set pages 226 and 227

5 - 7 - 7



y high-pressure tium lamps

short answer to this question is:

igh luminous efficacy iolden white light alanced colour rendering ong economic life teliable, stable operation excellent lumen maintenance short re-ignition time

h-pressure sodium lamps combine very h efficacies (up to 130 lm/W) with moderate our rendering, and are therefore suitable for ny applications where such factors, together h good economics and long lamp life, are portant.

Experience has shown that, since the late sixties when SON lamps were introduced on to the market, these light sources have proved themselves particularly in terms of all-round reliability. Compared with the version originally launched, today's high-pressure sodium lamps enjoy improved life, together with a higher light output and better lumen maintenance.

On top of this, the brief re-ignition time — the time taken for the discharge to restrike should an interruption in the mains supply occur represents an added safety feature; this interval is normally less than two minutes for lamps with an external ignitor in the circuit.



ne range at a glance

DN 50.W-I, 70 W-I - Two ovoid-shaped, ated lamps, each with a built-in ignitor and ed with an E27 base; for residential area hting and particularly for the conversion of ercury lamp installations.

ON 50 W-E, 70 W-E - Similar to SON 50 W-I d SON 70 W-I, except that the lamps require external ignitor.

ON 100 W, 150 W, 250 W, 400 W, 1000 W range of ovoid coated lamps suitable for a de selection of indoor and outdoor lighting plications; operate on a ballast plus an ternal ignitor; because of their ovoid shape, ese lamp types can also be used in optical stems designed for high-pressure mercury mps. SON-T 50 W-E, 70 W-E, 100 W, 150 W, 250 W, 400 W, 1000 W - Seven clear tubular lamps ideal for application in precise optical systems such as floodlights and road lighting luminaires; require a ballast and an external ignitor.

SON-S 150 W, SON-ST 150 W - High efficacy versions of the SON 150 W and SON-T 150 W lamps respectively.

SON-H 210 W, 350 W - Intended for direct replacement of mercury vapour lamps, the 210 W version can be connected to a 250 W mercury lamp ballast whilst the 350 W lamp connects to a 400 W mercury lamp ballast, without requiring an ignitor in the circuit; both lamps have ovoid, internally coated bulbs and an incorporated ignition aid. W-I - SON 70 W-I



w high-pressure sodium lamps

3

2

e heart of the Philips SON lamp stands the harge tube, fabricated from sintered ninium oxide. The tungsten electrodes and niobium supports are sealed into this tube a specially developed cement to give a ly reliable seal. During this process, the um, mercury and a rare gas (xenon for and SON-T, and neon/argon for SON-H) cilitate starting are also introduced into the

t, the tube is inserted into a clear, tubular elope (SON-T) or built into an ovoid bulb a diffusing layer (SON). Here it is held in be by the support wire. Extra protection is an by special support springs which hion the discharge tube against vibration. After these are fitted, the outer bulb is evacuated to minimise heat losses, a high vacuum being maintained by a getter which assists in ensuring maximum operating efficiency throughout lifetime.

9

8

6

5

10

11

SON lamps in the range are ovoid types where the bulb wall has been electrostatically coated with a very uniform layer of calcium pyrophosphate. The use of this diffusing powder results in very low light losses and guarantees constantly high quality performance during the life of the lamp. Added to that, there is less glare so that simpler and less costly optical systems can be employed.

Like all gas-discharge lamps the SON lamps require a current limiting device, plus an ignitor to ensure rapid, reliable starting. With the SON Ø)



0 W-I and 70 W-I and SON-H lamp types this inition device is built-in. Where the ignitor is xternal, a number of low-energy,

igh-frequency pulses are superimposed upon e mains voltage across the lamp electrodes.

he initial discharge takes place in a rare gas. eat is thus dissipated, causing some of the ercury to evaporate.

he sodium, with its lower excitation potential, nen gradually takes over the discharge and fter a short time the lamp burns stably, mitting its characteristic, pleasant,

olden-white light at luminous efficacies of up o 130 lm/W.

ome 80% of nominal light output is reached vithin an average of four minutes. An additional dvantage is the fast restrike time; for lamps vith an external ignition device, this factor can

be of the utmost importance in applications where short power supply interruptions might otherwise lead to dangerous situations owing to lack of light.

Cut-away view

- Porcelain insulating disc in base. 1.
- E27/E40 screw base. 2.
- Getter to ensure high vacuum throughout life.
 Internal ignitor for SON 50 W-I and 70 W-I, and SON-H.
- 5. Lead-in wire/support.
- 6. Expansion unit to eliminate temperature stresses on welds and discharge tube.
- 7. Inner phosphor coating.
- Translucent aluminium oxide discharge tube.
- 9. Tubular or elliptical outer bulb, impervious to atmospheric conditions.
- 10. Support/lead-in wire, twisted for improved optical characteristics.
- 11. Support springs.



tion

ressure sodium vapour lamps, for outdoor and indoor use, sintered aluminium oxide discharge tube enclosed in a outer bulb.

iption

cause of the high sodium pressure, the lamp combines ery high luminous efficacy with a good colour appearance. bulb wall is electrostatically coated with a very uniform

er of calcium pyrophosphate. e use of the coating results in very low light losses and sures constantly high quality performance throughout life. e geometry of the lamp makes it the ideal light source for a with the same reliable optical systems applied with

ditional advantages: ong economical life Excellent lumen maintenance Reliable, stable operation.

Applications

- **Public lighting**
- Parking lots
- Airports
- -Floodlighting
- Industrial lighting
- Plant irradiation
- Sports lighting ----

Ballasts and ignitors

High-pressure sodium lamps require high quality ballasts for optimum operation, as well as ignitors to ensure reliable ignition. For ballasts and ignitors see relevant leaflets.

Temperatures

Max. permissible base temperature: 250 °C Max. permissible bulb temperature: 350 °C

SON lamps

Dimensi	ions
---------	------

Lamp designation	A max.	B max.	C max.
SON 50 W SON 70 W SON 100 W SON 150 W SON-S 150 W SON 250 W SON 400 W SON 1000 W	156 156 186 227 227 227 292 400	35 35 43 53 53 53 53 58 60	72 72 77 92 92 92 92 122 168

.. ositions

data	
------	--

	Base	Min. supp for ignitior V	iy voltage יר ¹ }	Average lamp	Average lamp	Min. supply voltage for stable operation	Max. starting current (mains current)	Average Iuminous flux²) Im	Average luminance	Run-up time
		+20°C	—18°C⁴)	Voltage*) V	A	V	À	horizontal	cd/cm²	minutes*)
W-1 ⁵) W-E ⁵) W-E ⁵) W-E ⁵) W W W W	E27 E27 E27 E40/45 E40/45 E40/45 E40/45 E40/45 E40/45	198 198 198 198 190 170 170 170 170 170	220 220 220 200 200 200 200 200 200 200	85 85 90 100 100 100 100 100 105 110	0,76 0,76 1,00 1,20 1,80 1,80 3,00 4,45 10,30	200 200 200 200 200 200 200 200 200 200	1,08 1,08 1,35 1,35 1,70 2,40 2,40 4,50 6,50 14,00	3300 3300 5800 9500 13500 15500 25000 47000 120000	4,5 4,5 7 15 10 12 19 24 36	5 5 5 5 5 5 5 5 5 5 5 5 6

²) After 100 burning hours. er of minutes after which the lamp has reached 80% of its final luminous flux. I ignite even on nominal voltage at temperatures of—30°C. ernal ignitor, I with internal ignitor.

and packing data

			Packing uni	t		
1	Ordering number	Nett weight ka	Qty	Weight kg	Dimensions cm	Volume m ³
0 W-I 0 W-E 0 W-I 0 W-E 0 W 0 W 00 W	9281 508 088 9281 520 088 9281 501 088 9281 518 088 9281 516 088 9281 516 088 9281 510 098 9281 510 098 9281 520 098 9281 520 098	0,050 0,050 0,050 0,105 0,178 0,178 0,178 0,178 0,250 0,450	24 24 24 12 12 12 12 12 6 6	3,80 3,80 3,80 3,80 3,90 3,90 3,90 3,90 2,98 6,40	$\begin{array}{r} 44 \times 36 \times 39 \\ 45 \times 35 \times 30 \\ 44 \times 31 \times 35 \\ 58 \times 41 \times 47 \end{array}$	0,062 0,062 0,062 0,052 0,052 0,052 0,052 0,052 0,052 0,055 0,056 0,112







Lamp performance during starting period



50 W













finition

gh-pressure sodium vapour lamps, for outdoor and indoor use, h sintered aluminium oxide discharge tube enclosed in a ar, tubular hard-glass outer bulb.

escription

- Because of the high sodium pressure the lamp has a high luminous efficacy and a good colour appearance. The clear, tubular outer bulb makes this light source highly suitable for use with specially designed optical systems. Additional assets: • Long'economical life
- · Excellent lumen maintenance
- Reliable, stable operation.

Applications

- Public lighting Parking lots
- ----
- Airports _ -----
- ____
- Floodlighting Industrial lighting Plant irradiation -
- Sports lighting

Ballasts and ignitors

High-pressure sodium lamps require high quality ballasts for optimum operation, as well as ignitors to ensure reliable ignition. For ballasts and ignitors see relevant leaflets.

Temperatures

Max. permissible base temperature: 250 °C Max. permissible bulb temperature: 450 °C

SON-T lamps





Lamp performance during starting period



lamp wattage lamp voltage lamp current luminous flux Wia Via Iia Φ =





Effects of mains voltage variations





10 and 20% fewer luminaires would be required when using Solarcolour Plus, compared when OLOUR PLUS LAMPS

Jehting Design Lumens 000 hrs	26500	35000 -	47000	1
Initial Lumens 100 hrs 2	28000	37000	50000	
Std Pack	10 m	- 01		and the stand of the stand of the stand
3	R12.55	R12.55	HIZ-55	Testanosti
Nomina Nomina Supply Volts	220	220	077	and a series and a series of the series of t
Watts	250		2.74	



(with starter) Reflector SON-R

	12032
Lighting Design Lumens 2000 hrs	21500 22500 34000 34000
Initial Lumens 100 hrs	23000 31500 37000 42500
Std Pack	1 @ 310W
Cap	E40 (GES) E40 (GES) E40 (GES)
Minimum Nominal Suppiy Volts	220 220 230 230
Watts	250 310/250 400



1000 m	4 3.1.5 3.1.5		P) (4

using Solarcolour Plus, compared in inger life and improved iuman lamps. Suttable external starters ar			
miss would be required when imps of the same writinge. Lo these second generation SON	and the second se	(without starter)	
dard high pressure sodium la iterance are also featured of ined with Plus lamps.		r Tubular SONP-T	Minim:

Lighting

Lighting Design Lumens 2000 hrs	17000 32500 400% 58000
Initiai Lumens 100 hrs	17520 33000 41000 56500
Pack Pack	- 10 - 10 - 10 - 10 - 10 - 10 - 10 - 10
Cap	E40 (GES) E40 (GES) E40 (GES) E40 (GES)
Nominal Supply Voits	220 220 220
Watts	150 250 250 200

Eiliptical Diffused SONP-E $\langle E \rangle$ (without starter)

15006	3:000	J Jesto	53500	
10 16500	10 31500	10	10 53000	
E40 (GES)	E40 (GESI	140 (CEV	EdU (GES)	
220	220	0.77	770	
150	003	ACC	227	

SOLARCOLOUR DE LUXE LAMPS

compared with standard lamps, some of the yellow radiation is converted tow ards the red and one ends Improved colour rendering is the main benefit of De Luxe lamps. With increased sodium pressure

<

1	Lighting Design Lumens 2000 hrs		1997	11600 20000 34500
tarter)	Initial Lumens 100 hrs	12500 23780 38500	arter}	12000 21750 37000
without st	Std Pack	10 10 10 10	without st	10 10
T E	Cap	E40 (GES) E40 (GES) E40 (GES)	DL-E	E40 (GES) E40 (GES) E40 (GES)
lar SONDL-	Minimurn Normanal Supply Voits	220 220 220	ffused SON	220 220 220
Clear Tubu	Watts	150 250	Elliptical Di	150 250 400

Manufactured to IEC602

For details of control gear see pages 166 and 167 and section 13. For full technical specification see pages 226 and 227

- man

F y full (achinal specifications see pages 226 and 227

えしていますちょ

transformed to FE602









	474					
RING DATA		Ordering number				
ation	Forlamps	Narrow beam	Wide beam	Asymmetrical beam	Weight kg	
	1 x SON-T 250 W	9112 702 302	9112702303	-	7,3	
)3	1 x SON-T 400 W or 1 x HPI-T 400 W	9112 702 448	9112702449	9112 702 428	7,3	
3G	1x SOX 35 W	91127056002)			9,1	
HNF 00	3	9119270007	9119270007	9119270007	1,4	

DATA

T 250 W narrow beam



Light distribution diagrams











N/T 400 W wide beam

30^o 15^o 15^o 30^o 15^o 30^o 40^o 40^o

Isocandela diagrams







ICAL WIRING DIAGRAMS

p ast

acitor or



MP	2 x HPI(-T) 400 W	
oltage current ng current ors	220 V - 50 Hz 2 x 3,00 A 2 x 2,00 A 2 x 30 µF / 250 V ≧ 0,85	

I(-T) 150 W	SON	(-T) 250 V	W SON(-T) 400	W SON(-T) 100	W OC	
	 I					
	4	*	SON(-T) 150 W	SON(-T) 250 W	SON(-T) 400 W	SON(-T) 1000 W
voltage g current ting current itor			220 V - 50 Hz 1,00 A 0,85 A 20 µF / 250 V ≧ 0,85	220 V - 50 Hz 2,30 A 1,40 A 36 µF / 250 V ≧ 0,85	220 V - 50 Hz 3,60 A 2,20 A 45 µF / 250 V ≧ 0,85	220 V - 50 Hz 9,30 A 5,60 A 100 µF / 250 V ≧ 0,85



FOR LAMP	1 × SOX 90 W	· · · ·
Mains voltage Starting current Operating current Capacitor Cos φ	220 V - 50 Hz 0,57 A 0,50 A 9,6 µF / 300 V ≧ 0,85	

ĝ