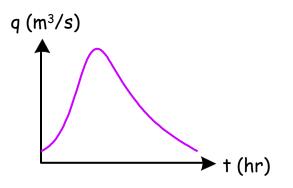
# Chapter 3 Hydrograph Analysis

# Hydrograph Analysis

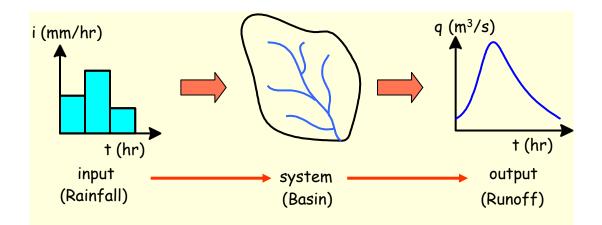
- Components of Runoff
- e Hydrograph Characteristics
- Onit Hydrograph Theory
- Synthetic Unit Hydrographs



- The major characteristics of streamflow are:
  - its volume for a certain duration (month or year)
     different uses & storage
  - its extreme values



# Hydrograph Analysis



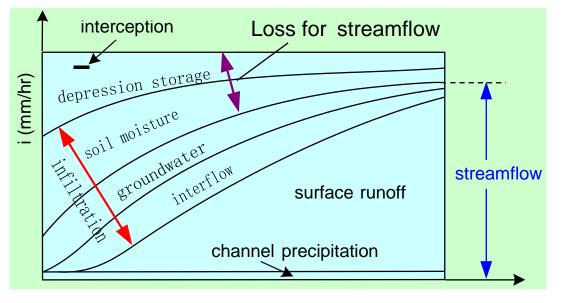
#### Components of Runoff

- Channel Precipitation
- Surface Runoff
- Interflow
- Groundwater Flow

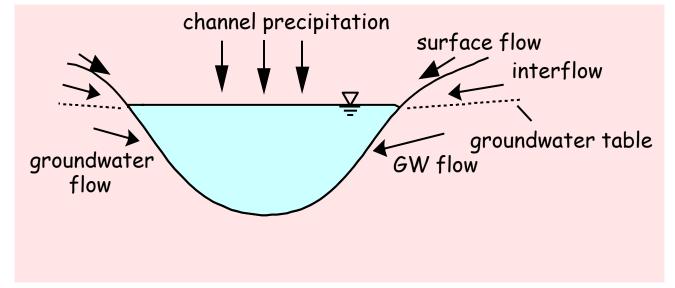
- Interception, depression storage, soil moisture are LOSSES for streamflow.
- The other portions of precipitation reach streams sooner or later.

## **COMPONENTS OF RUNOFF**

#### In a rainfall block

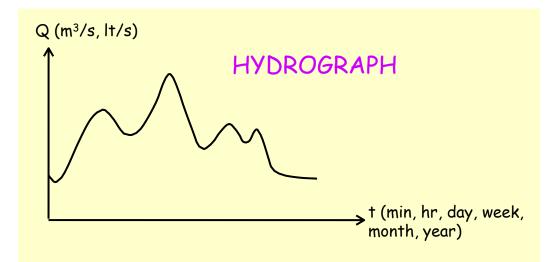


In the channel



# Hydrograph

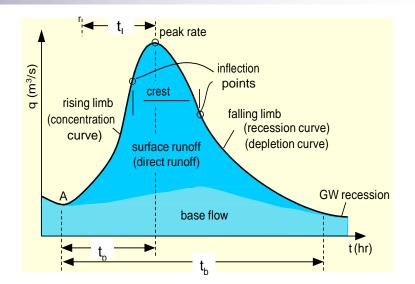
- e Hydrograph → discharge vs time
   (m<sup>3</sup>/s, lt/s) (min, hr, day, month, yr)
- Sometimes plotted as stage vs time.



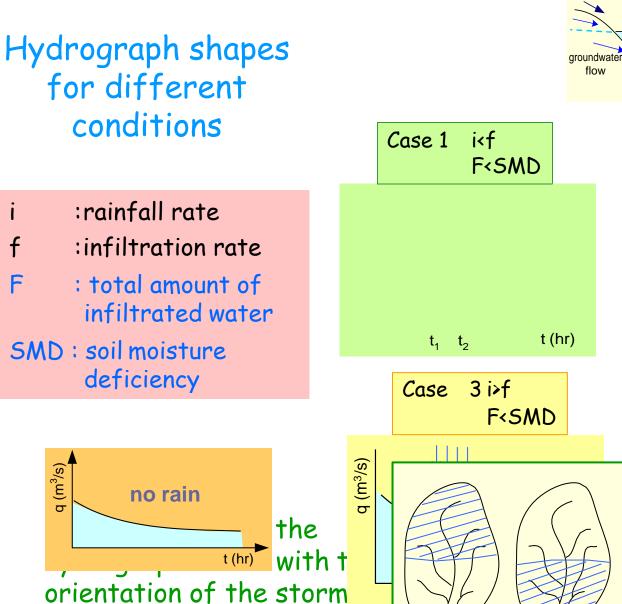
The comparison of hydrographs with the corresponding rainfall hyetographs provides a lot of information about the rainfall-runoff relation of the basin.

## Hydrograph

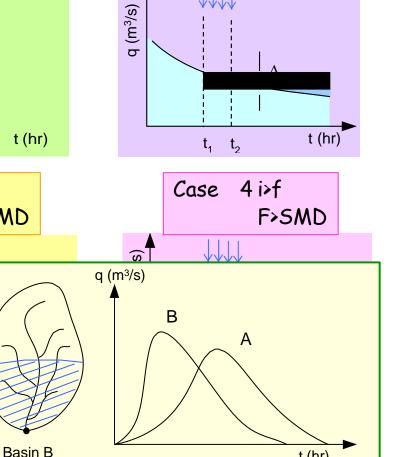
The crest of the hydrograph is governed by the duration of rainfall.



- Shape of the rising limb = f(rainfall intensity & basin characteristics s.a. infiltration capacity, shape, slope, etc.)
- Shape of falling limb = f(basin characteristics s.a. depression, surface & subsurface storages)
- Characteristics of the rainfall do not impact the falling limb since recession starts after the end of the rainfall.



Basin A



channel precipitation

Case 2

flow

surface flow

GW

flow

i<f

F>SMD

interflow

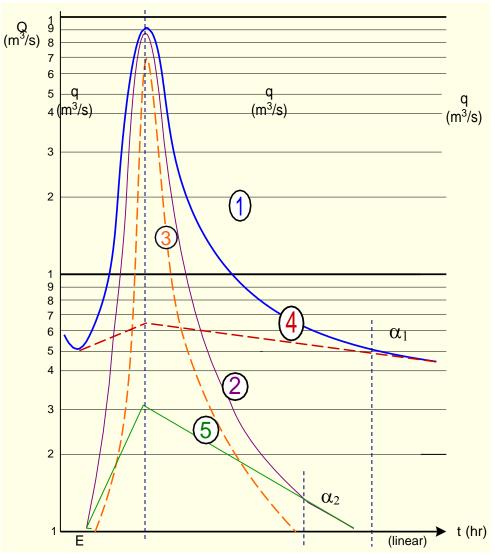
groundwater

table

## Hydrograph Separation Techniques

- Separation line between surface runoff & baseflow is not definite & varies widely depending on the existing conditions.
- Inaccuracies in separation are not very important for many storms, since the max. rate of discharge is only slightly affected by the base flow.
- @ Methods for seperation:
  - Simple Method
  - Approximate Method
  - Barnes (Semi-log) Method

### Seperation Methods



#### 1. Barnes (Semi-log) Method

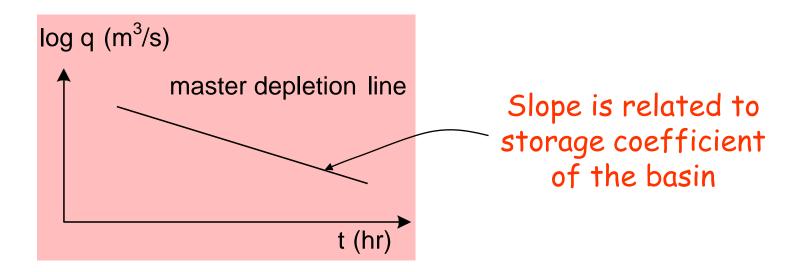
Total flow (SF+SSF+BF) (1  $q = q_0 e^{-\alpha_1 t}$ Base flow (BF) (4) (SF+SSF) (1) – (4) (2)  $q = q_0 - \alpha_2 t$ (5) Subsurface flow(SSF) Surface flow (SF) (2) - (5) $(\mathbf{3})$ 

#### Master depletion curve (representative depletion curve)

$$q = q_0 e^{-\alpha t}$$

$$\log q = \log q_0 - t \alpha \log e$$

$$y = a + bx \text{ (straight line on semi-log paper)}$$



## Unit Hydrograph (UH) Theory

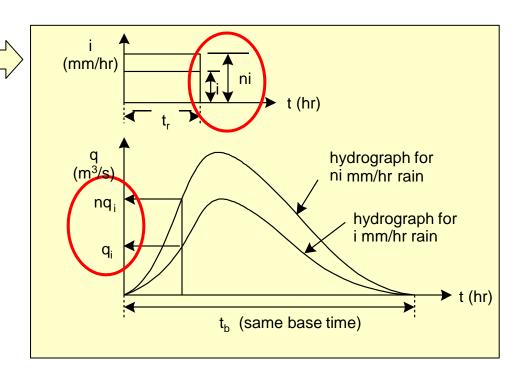
- Hydrograph of surface runoff (direct runoff) resulting from 1 cm of excess rainfall which is uniformly distributed over basin area at a uniform rate during a specified period of time.
- Q Depth = 1 mm for arid or semi-arid regions or if basin is small.
- @ Given by Sherman in 1932.
- It is assumed that the UH is representative for the runoff process of a basin.
- @ Baseflow should be separated from total flow to find direct runoff, and all the losses should be subtracted from total precipitation before any analysis.

# Unit Hydrograph (UH) Theory

- OH assumptions:
  - 1. Excess rainfall is uniformly distributed within a specified period of time.
  - 2. Excess rainfall is uniformly distributed over the basin area.
  - 3. Base time of direct runoff is constant for a specified duration of rainfall.
  - 4. Ordinates of direct runoff hydrograph are directly proportional to the total amount(depth) of direct runoff ( = depth of excess rainfall) for the same duration rainfalls.
  - 5. Unit hdrograph is unique for a basin.

1. Linearity assumption

(Principle of superposition, Principle of proportionality)

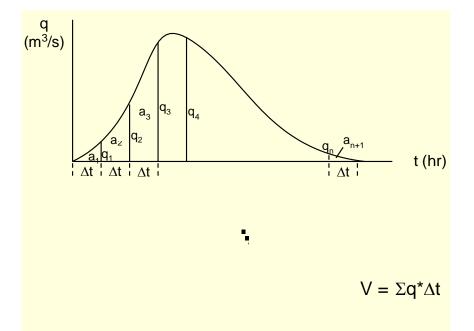


#### 2. Principle of time-invariance

When basin characteristics change  $\rightarrow$  UH changes

## Unit Hydrograph

@ The unit hydrograph is denoted as dUH<sub>t</sub> ( d in cm, t in hr)
 @ The depth of flow for a hydrograph → the area under the hydrograph.



$$d = \frac{V}{A} = \frac{\int q \, dt}{A} = \frac{\sum q * \Delta t}{A}$$

 $\sum q =$ sum of ordinates of the hydrograph (m<sup>3</sup>/s)

$$d_t = time interval (s)$$

A = basin area 
$$(m^2)$$

$$d = depth(m)$$

Figure 7.18 Determination of volume of runoff

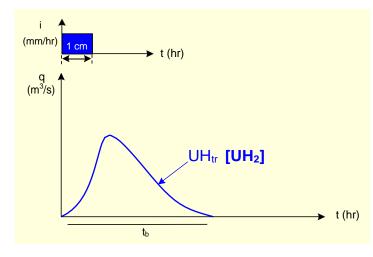
#### Unit Hydrographs of Different Durations

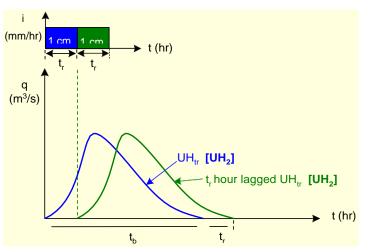
- There are 2 methods to obtain UHs of different durations for a basin when a UH of certain duration is known
  - The lagging method
  - S-curve method

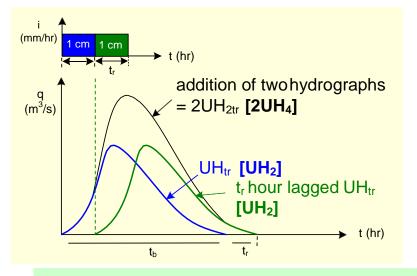
#### The Lagging Method

- Q A UH of certain duration can easily be obtained by using the lagging method if a UH of different duration is known for the basin.
- The only condition is that the durations be multiples of each other.

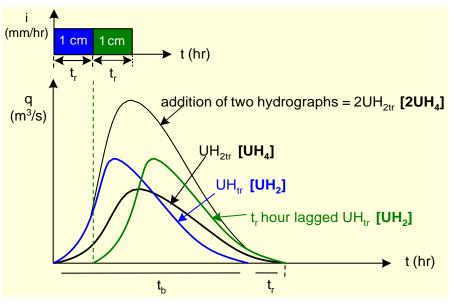
## HYDROGRAPH ANALYSIS - lagging method



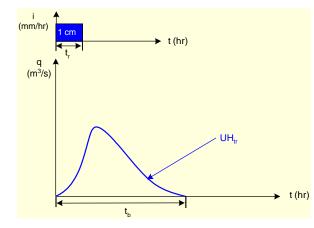


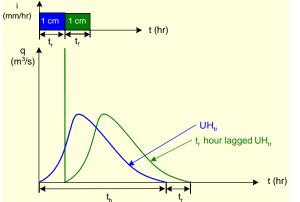


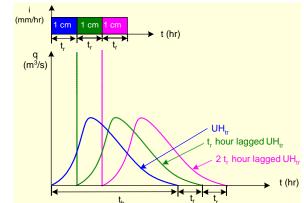
 $UH_2$  + (2 hr lagged)  $UH_2$  =  $2UH_4$ 

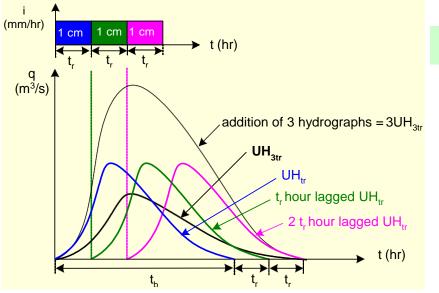


### HYDROGRAPH ANALYSIS - lagging method









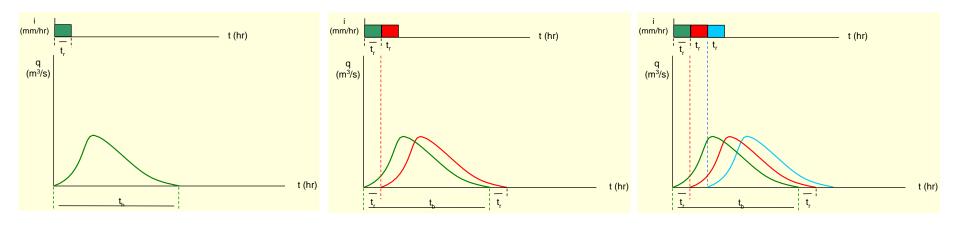
 $UH_t$  + (t hr. lag)  $UH_t$  + (2t hr.lag)  $UH_t$  =3 $UH_{3t}$ 

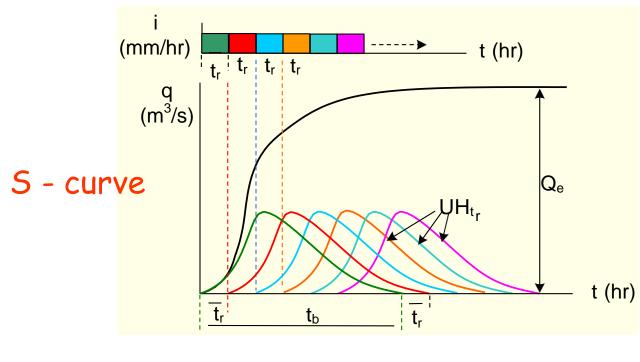
As 
$$t_r$$
 tes  $q_p \downarrow es$   
 $t_p$  tes  $t_b$  tes

## The S-Curve Method

- It is used to obtain UHs of different durations that are not multiples of each other.
- S-curve is the hydrograph that would result from an infinite series of UHs of t<sub>r</sub> durations, each delayed t<sub>r</sub> hours wrt the preceding one.
- In other words, it is the hydrograph of the runoff of continuous rainfall with an intensity of 1/t<sub>r</sub>.
- S-curve has the form of a mass curve, the discharge of the basin becoming constant after the time of concentration.
- Thus each S-curve is unique for a specified UH duration, in a particular drainage basin.

S - Curve





$$n = t_b/t_r$$
  
 $Q_e = i * A (mm/hr * km^2)$   
 $Q_e = d/t_r * A = 1/t_r * A$   
 $(d= 1 \text{ cm})$ 

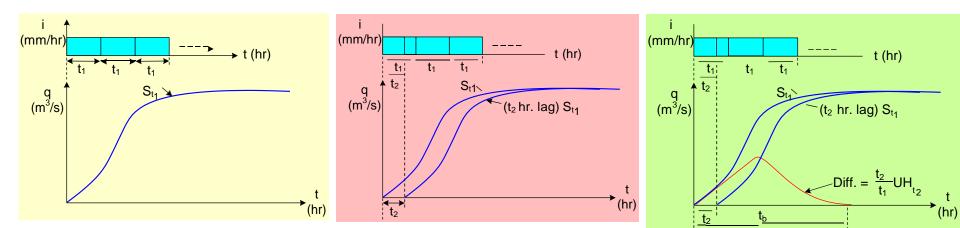
$$Q_{e} = 2.78 \frac{A}{t_{r}}$$

Q<sub>e</sub> = constant outflow (m<sup>3</sup>/s) A = area of basin (km<sup>2</sup>) t<sub>r</sub> = duratio of UH (hr)

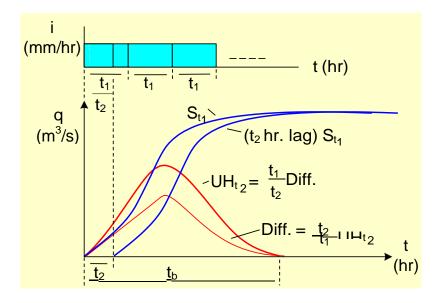
## S - Curve

- Q There may be fluctuations around the constant flow Q<sub>e</sub> due to a number of reasons.
  - One of them may be the duration of effective precipitation, t<sub>r</sub>.
    - It may be shorter or longer than the actual effective precipitation duration with uniform intensity.
  - Another one may be the uneven distribution of rainfall in the basin or nonlinearities in the system.

#### Obtaining UH using S-curve $(t_2 < t_1)$



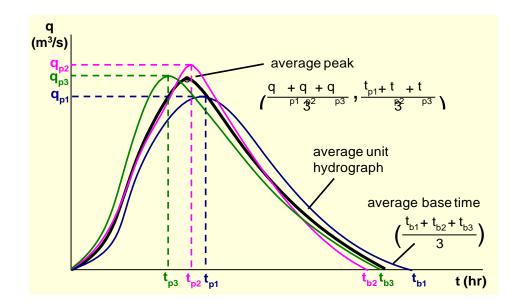
Diff. = 
$$S_{t1} - (t_2 \text{ h.l.}) S_{t1}$$
  
Diff. =  $(t_2 \cdot 1/t_1) UH_{t2} = t_2/t_1 UH_{t2}$   
 $UH_{t_2} = \frac{t_1}{t_2} [s_{t_1} - (t_2 \text{ hr. lag}) s_{t_1}]$ 



- Q 7. Determine the representative UH for the basin by averaging
  - the peak flows,
  - times to peak, and
  - time bases of the UHs.

The average UH is then sketched following the shapes of the individual hydrographs.

8. Adjust the area under the curve to unit depth.



#### **Example** $UH_1$ of a basin is given.

Determine  $UH_2$ ,  $UH_3$  and area of this basin by lagging method

	Time (hr)	UH1 m³/	1 hr.lag UH1	2UH	UH	2 hr.lag UH1	3UH₃	UH		
	0	0	1	0	0	· · · · ·		3		
	1	12		12	6		0	0		
	2	36	0	48	24		12	4		
	3	24	12	60	30	0	48	16		
	4	18	36	42	21	12	72	24		
	5	12	24	30	15	3	78	26		
	6	6		18	9	<u> </u>			-	
	7	0	18	6	3		54	18		
	8		12	0	0	4 18	36	12		
	9		6			12	18	6		
			0			6	6	2		
						0	0	0		
	Σq	108			108			108	•	
				l	$\Sigma q^* \Delta t$	. <b>A</b>	$\Sigma q^*$			
$UH_1 + (1 \text{ hr. lag}) UH_1 = 2 UH_2 \qquad \qquad d = \frac{\sum q^* \Delta t}{A} \rightarrow A = \frac{\sum q^* \Delta t}{A}$										
U  + (1 hr   aa )   U  + (2 hr   aa )   U  = 2   U										
	. (	. lug, off	1 ' ( <b>~</b> '''. ''	$108*1*3600 = 38.88*10^6 \text{ m}^2$						

 $A = \frac{108*1*3600}{0.01} = 38.88*10^6 \text{ m}^2 = 38.88 \text{ km}^2$ 

Δt

# **Example** $UH_1$ of a basin is given.

Determine UH<sub>2</sub> and UH<sub>3</sub> of this basin by S-curve method

t (hr)	UH1	1 h.l UH <sub>1</sub>	2 h.l UH <sub>1</sub>	3 h.l UH <sub>1</sub>	4 h.l UH <sub>1</sub>	5 h.l UH1	6 h.l UH1	<b>S</b> <sub>1</sub>	2 h.l S <sub>1</sub>	dif f	UH	3 h.l S <sub>1</sub>	dif f	UH <sub>3</sub>
0	0							0		0	0		0	0
1	12	0						12		12	6		12	4
2	36	12	0					48	0	48	24		48	16
3	24	3	12	0				72	12	60	30	0	72	24
4	18	2	36	12	0			90	48	42	21	12	78	26
5	12	18	24	36	12	0		102	72	30	15	48	54	18
6	6	12	18	24	36	12	0	108	90	18	9	72	36	12
7	0	6	12	18	24	36	12	108	102	6	3	90	18	6
8		0	6	12	18	24	36	108	108	0	0	10 2	6	2
9			0	6	12	18	24	108	108			10	0	0

$$\begin{array}{ll} \mathsf{VH} = \frac{1}{2} \begin{bmatrix} \mathsf{S} - (2 \, \mathrm{hr.lag}) \, \mathsf{S} \end{bmatrix} & \mathsf{UH} = \frac{1}{3} \begin{bmatrix} \mathsf{S} - (3 \, \mathrm{hr.lag}) \, \mathsf{S} \end{bmatrix} \\ \mathsf{H} = \mathsf{T} & \mathsf{H} = \mathsf$$

UH<sub>t<sub>2</sub></sub> =  $\frac{t_1}{t_2} [s_{t_1} - (t_2 \text{ hr. lag}) s_{t_1}]$ 

## Synthetic Unit Hydrograph

- Snyder Method
- e SCS Method

(developed by Soil Conservation Services, 1957)

- e Espey Method
- Mockus Method
- OSİ Synthetic Unit Hydrograph Method
- Time Area Method